

Genetic algorithm based Ku-band microstrip patch antennas optimization to avoid jamming attacks

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Abstract—Genetic algorithm (GA)-based antenna design has been shown to efficiently improve its electrical properties. This endeavor addresses design and optimization of patch antennas. Two different methods were conducted. First, optimization was carried out over the whole antenna extension. Second, half antenna was optimized and the final design was obtained by reflection. The optimization process was conducted using Genetic Algorithm (GA), return loss was obtained with full wave Finite-Differences Time-Domain (FDTD-3D), and the initial configuration (design) was obtained with line transmission and cavity method. All methods implemented in-house software. The antenna was designed to operate in Ku band with the center frequency at 16 GHz. Antenna with return greater than 22dB and bandwidth between 2-5 GHz, were obtained. The effectiveness of the proposed designs is confirmed through proper simulation results. The minimization of the side lobe. Such optimization would aim to make a communication system more robust to Electronic Warfare attacks.

Keywords—genetic algorithms, jamming attacks, microstrip antenna, satellite communications.

I. INTRODUCTION

The rapid advancement in the satellite communication field in the past few decades has led to the development of small, low profile and efficient antenna design. Antenna is an important structure in any satellite communication system. Services such as satellite internet access, spacecraft telemetry, command, and tracking communications [1], has boosted research in this field, and efficient antennas definitely improves the overall performance of the system.

However, electronic warfare (EW) attacks on ground stations are a growing threat to government, military and commercial satellite communications. In these attacks, adversaries use electromagnetic energy to disrupt or deny friendly access to radio frequency (RF) communications. The forms of electronic warfare are deployed to disrupt and impede operations by interfering with the transmission of RF signals between satellites and ground stations [2] [3] [4]. Reducing the antenna's side lobe is always an important goal to prevent attacks in satellite communications [5] [6] [7].

This work investigates microstrip antennas for reduce the side lobe satellite communication systems, due to its advantages compared to other antennas, such as large single-dish [8]. Various schemes are being used to minimize the drawbacks of this type of antennas, but it is a difficult task. In this work,

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the antenna was designed to operate in Ku band with the center frequency at 16 GHz, the frequency band (15.25 - 17.25 GHz). This work used the genetic algorithms to overcome these disadvantages, based on references [9] [10] [11]. Specifically the numerical method FDTD-3D was combined with the genetic algorithm GA for bandwidth and return loss optimization. The initial design was obtained used the resonant cavity / transmission line methods [12], All methods implemented in-house software.

Antenna design using FDTD-3D is described in section 2. Section 3 presents aspect related with Genetic Algorithms used in this work. Section 4 shows the present numerical results. Finally, section 5 presents the conclusions and achieve some goals. The effectiveness of the proposed designs is confirmed through proper simulation results.

II. FDTD-3D METHOD

The FDTD-3D method [13], [14] with the “Uniaxial Perfect Matched Layer” (UPML) [15] was used.

A. The source

The Morlet wavelet function was used. Input signal is given by the equation: (1)

$$E_z(t) = E_0 e^{-2\pi f_b(t-t_0)^2} \cos(2\pi f_c(t-t_0)) \quad (1)$$

where $E_0 = 22 \text{ V/m}$ is the signal amplitude, $t_0 = 5.02 \text{ ns}$ is the time at which the pulse reaches its maximum value, $f_c = 16 \text{ GHz}$ is the central frequency, $f_b = 2 \text{ GHz}$ and t between $[0, 8000\Delta t]$ represents the propagation time signal with $\Delta t = 0.0342 \text{ ns}$ representing the value of the time step. Figure (1) shows the time domain signal and its frequency domain equivalent.

B. Scattering parameter

Microstrip patch antenna is a one-port circuit. Its scattering matrix has only one element, that is, S_{11} or the reflection coefficient. The electromagnetic field at any time obtained using FDTD is the superposition from incident and reflected signals. In order to compute the input signal, the network is simulated first without the presence of the patch. Since there is no reflection at the port position, the recorder signal corresponds to the input signal. After the calculation of input signal at port 1, FDTD simulation can be performed a second time with the patch

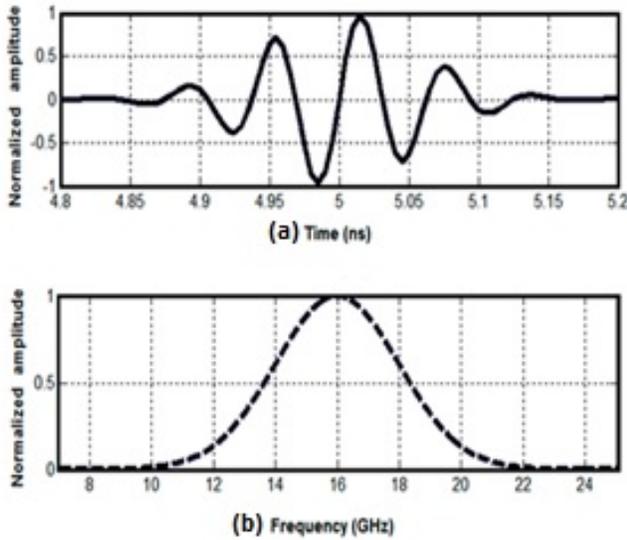


Fig. 1. Wavelet function for excitation: (a) time domain and (b) frequency spectrum.

present, resulting in the total electromagnetic field. The reflected signal at the port is the subtraction of the total signal from the input signal (obtained in the first simulation). Frequency domain responses of the system are calculated by performing Direct Fourier Transform to the simulated time-domain signals.

In this work, the traditional procedure has been implemented, with changes in the application related to the evolution process. Whereas it is generated a different patch at each genetic generation, the line-feed does not suffer any modification. The first step in the calculation of return loss is the same for all antenna configurations. It is performed only once and the results are used in other generations.

III. GENETIC ALGORITHMS

The genetic algorithm [16] begins by considering the rectangular microstrip antenna with inset geometrically designed using the transmission line method and resonant cavity [12] (Figure 2).

Afterwards, the patch is modified using GA, for which were considered two schemes: using the total area of the patch; and with the left half of the patch, symmetrically mirrored to the right.

For the first antenna, where the total area of the patch was used, the patch parameters values (Figure 2) are: $W = 11.68 \text{ mm}$, $L = 8.87 \text{ mm}$, $W_f = 1.40 \text{ mm}$, $g = 0.70 \text{ mm}$, $Y_0 = 0.88 \text{ mm}$, substrate dielectric constant = 2.2, substrate height = 0.45 mm , substrate width = 16.58 mm , substrate length = 23.70 mm , the height of ground plane, height of the patch and height of line feed were taken as one delta mesh in the z direction.

The patch was divided into a binary matrix of 17×17 sub-patches, as shown in Figure (3). The sub-patch in this

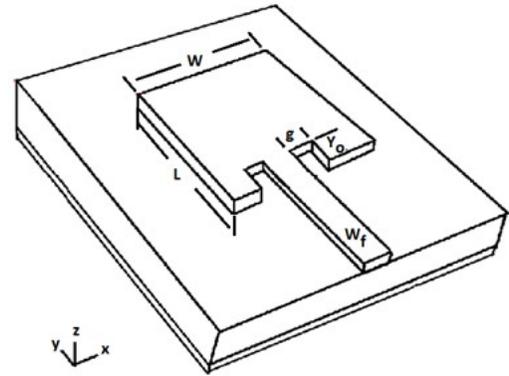


Fig. 2. Initial microstrip antenna design.

representation is an intrinsic representation of problem, this indicates presence (set as 1) or absence (set as 0 - not printed) of copper sub-patches in candidate solution (chromosome).

The size of the population was set to 70 chromosomes. For the chromosome, various sizes were tested, but a digital individual of 289 elements (connect rows of the matrix) was chosen. The fitness function, related to the bandwidth and the return loss, is presented in equation (2).

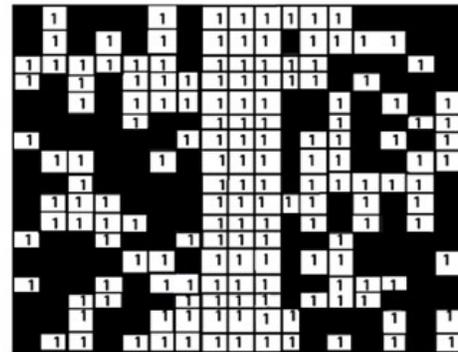


Fig. 3. Modified patch antenna.

$$fit = \alpha fit_{BW} + (1 - \alpha) fit_{RL} \quad (2)$$

Two optimization objectives were used. In Equation 2 α is a weighting factor in the range $[0, 1]$ which allows the choice of the emphasis or preference of a parameter with respect to each other. The fitness function related to bandwidth (fit_{BW}) is set with minimum bandwidth 2.0 GHz , and the related to return loss (fit_{RL}) demand further loss of 25 dB .

After the initialization of population and definition of the fitness function, the cyclic or evaluative process begins (cycle and generation are effectively interchangeable terms in this work). In the cycle process a roulette-wheel technique was used. Shuffle crossover with swapping probability was set equal to 0.5. The mutation probability was fixed to 0.001 and bit-flip [11].

For the second and third antennas (Figures 6, 7) the left half of the patch and symmetrically mirrored the right was considered.

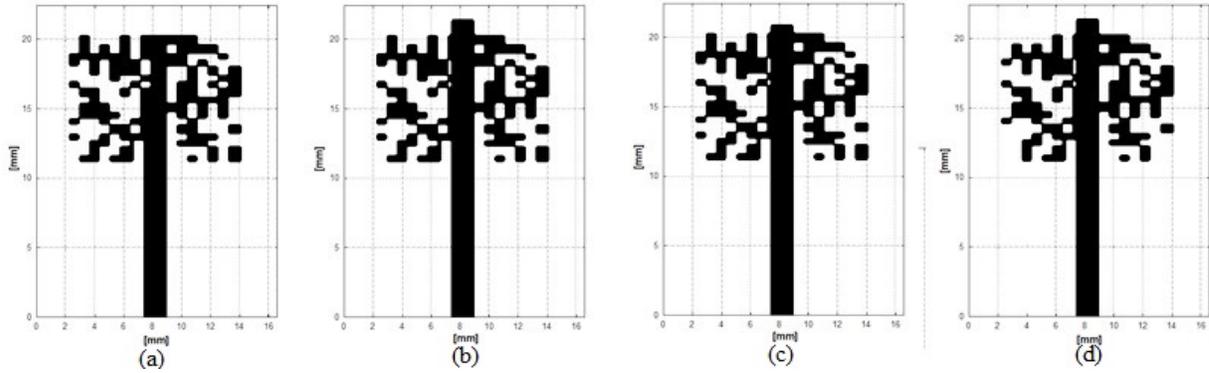


Fig. 4. Changes in the antenna (4) in the evolutive process.

The dimension of the second and third antennas (Figures 6, 7) are: $W = 12.81 \text{ mm}$, $L = 14.23 \text{ mm}$, $W_f = 1.42 \text{ mm}$, material substrate value = 2.2, height substrate = 0.45 mm , width substrate = 23.48 mm , length substrate = 28.23 mm , the height of ground plane, height patch and height of line feed were taken as one delta mesh in the z direction.

IV. NUMERICAL RESULTS

For the three rectangular microstrip antennas (4, 6, 7), the first was built with an inset and the other without it. To work in the Ku band, the initial dimensions were obtained by the resonant cavity and transmission line methods. The calculation of return losses was obtained with the FDTD-3D method. In the optimization process, in order to provide higher bandwidth (compared to the original antenna), genetic algorithm was used.

Figure (4) shows several steps in the evolutionary process of the first antenna, chosen in order to leave evidence of some important characteristic in the optimization process. In Figures (4.b-4.d) for instance, the line feed has been extended beyond the top edge of the patch, at different multiples of Δy , and the current flows from the line to the sub-patches (it forms a resonant structure). On the other hand, the subpatches that did not pair directly became parasitic sub-folders. In common antennas it is known that these elements improve its bandwidth. The return loss for the partial stages of the first antenna is presented in the Figure (5). The antenna in Figure (4.a), represented by a discontinuous line in the Figure, has a bandwidth of 2.83 GHz and a return loss of 34.85 dB . The antenna in Figure (4.b) has a bandwidth of 4.80 GHz with a return loss of 23.45 dB , represented by a continuous line.

The antenna in Figure (4.c) has a bandwidth of 3.84 GHz and a return loss is 25.05 dB , represented by a continuous line with 'x'. The antenna in Figure (4.d) has 4.80 GHz of bandwidth and a return loss of 39.42 dB , represented with a continuous line with 'o'. The antenna in Figure (4.d) is the final stage of the optimization process.

The antenna in Figure (4.b) presents the worst return loss if compared with the antenna in Figure (4.a), but it presents wider bandwidth, approximately 4.80 GHz . These changes are due to the mutation process, particularly in the extension beyond the upper edge of the patch (feeding line, in 4 sub-patches).

Comparisons between Figures (4.c) and (4.d) show that the bandwidth of the antenna in Figure (4.d) is larger than that of the antenna in Figure (4.c), and that the antenna in Figure (4.d) shows a better return loss.

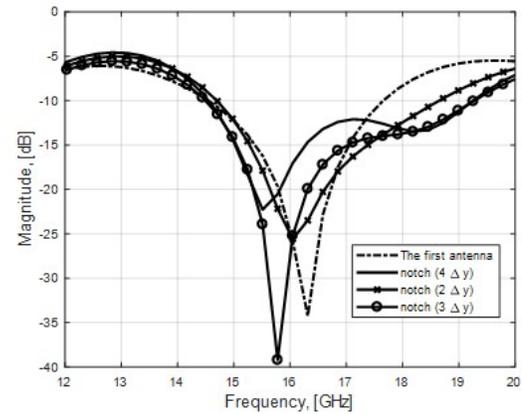


Fig. 5. Return loss Comparison of partial results of the optimization process.

In Figure (5) it is also possible to relate the performance of the antenna with the size of the notch. These small changes are characteristics of the mutation process. It should be emphasized that for the antenna in Figure (4.d), the bandwidth has been increased by approximately 2 GHz and the return loss by 5 dB if compared to the antenna of Figure (figChangesAntenna.a), after the optimization process.

The antennas in Figures 6 and 7 were obtained by mirroring the left half of the patch in order to obtain a symmetrical structure and to observe the effects of this symmetry. The return loss presented in the Figure (8) correspond to these symmetric antennas.

Figure (8) presents the final result of the optimization process for both antennas. Notice that in the antenna of Figure (6) the feed line has an extension beyond the upper edge of the patch. The presence of this discontinuity allows the band and the return loss to increase. The extension beyond the upper edge of the patch produces negligible changes in the parameters to be optimized. The bandwidth of the antenna of Figure (6) is 4.97 GHz with a return loss of 27.12 dB . In the antenna

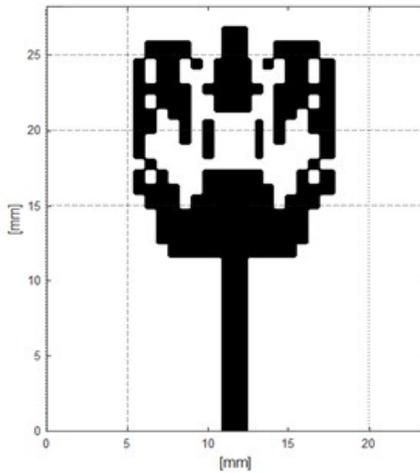


Fig. 6. First symmetric antennas.

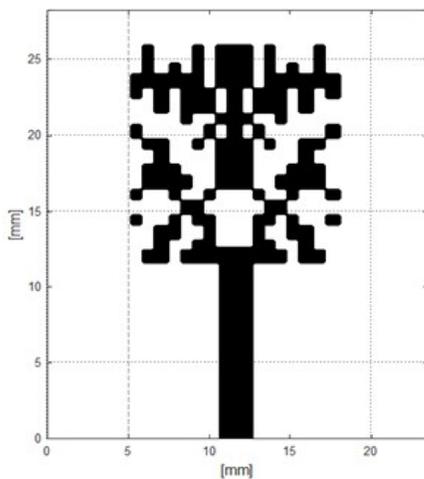


Fig. 7. Second symmetric antenna.

of Figure (7) the feed line presents an extension between 12.81 mm and 16.37 mm . The antenna bandwidth is 5.0 GHz and its return loss is 27.20 dB .

Figure (9) presents the radiation patterns of the antenna of Figure (7) for 15.25 , 16 and 17.25 GHz .

V. CONCLUSION

Evaluation of the article entitled Genetic algorithm based Ku-band microstrip patch antennas optimization to avoid jamming attacks was made. The objective of the article was to investigate the optimization of an antenna design through the minimization of the side lobe. Such optimization would aim to make a communication system more robust to Electronic Warfare attacks, since a satellite communication link is easily exposed to a jammer or a signal interceptor, it must be protected to overcome the hostile attacks.

This paper presented the design of compact and efficient microstrip patch Ku-band antennas to avoid jamming attacks.

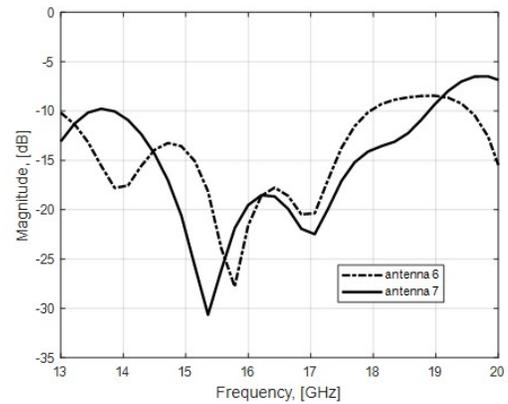
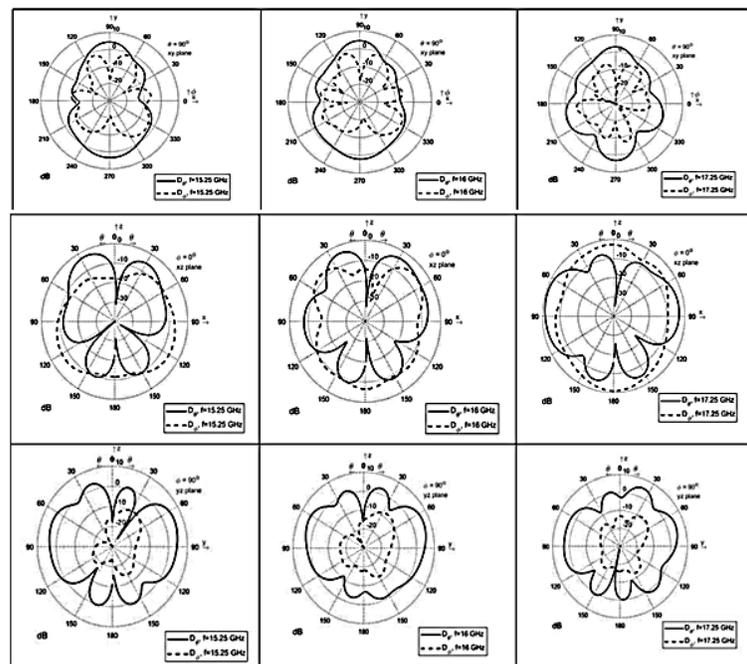


Fig. 8. Return loss comparison for two symmetric antenna.


 Fig. 9. Radiation patterns of the antenna of Figure (7) for 15.25 , 16.0 and 17.25 GHz . Planes xy , xz and yz

Return loss greater than 30 dB with a bandwidth up to 5.0 GHz were obtained. When compared to the rectangular patch antenna, return loss was increased by 14.2% and bandwidth by 85.0% , which can decrease its side lobe and then make the hostile site difficult to interfere or intercept.

After the optimization process non restricted configurations were obtained. This process can potentially generate a variety of structures that cannot be conceived by conventional design approaches. The advantages of the proposes antenna are lower complexity and easy implementation that could be used to provide further protection from jamming.

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